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Abstract

Compared to $\text{Pb}(\text{Zr}_{1-x}\text{Ti}_x)\text{O}_3$ (PZT) polycrystalline ceramics, relaxor-PT single crystals offer significantly improved performance with extremely high electromechanical coupling and piezoelectric coefficients, making them promising materials for piezoelectric transducers, sensors and actuators. The recent advances in crystal growth and characterization of relaxor-PT-based ferroelectric single crystals are reviewed in this paper with emphases on the following topics: (1) the large crystal growth of binary and ternary relaxor-PT-based ferroelectric crystals for commercialization; (2) the composition segregation in the crystals grown from such a solid-solution system and possible solutions to reduce it; (3) the crystal growth from new binary and ternary compositions to expand the operating temperature and electric field; (4) the crystallographic orientation dependence and anisotropic behaviors of relaxor-PT-based ferroelectric crystals; and (5) the characterization of the dielectric, elastic and piezoelectric properties of the relaxor-PT-based ferroelectric crystals under small and large electric fields.

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Review

Advances in the Growth and Characterization of Relaxor-PT-Based Ferroelectric Single Crystals

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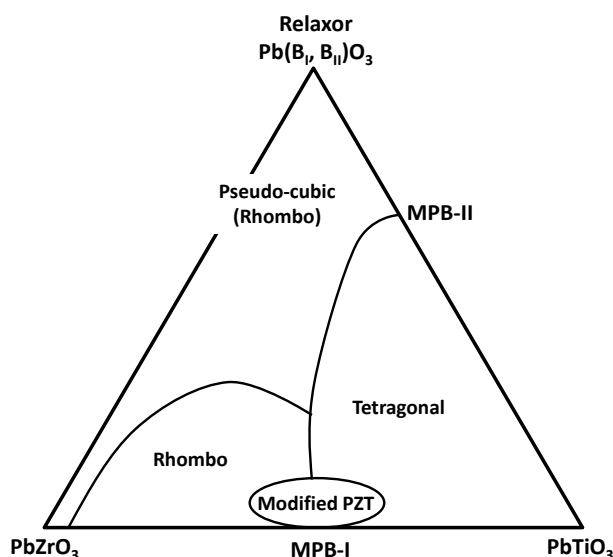
Abstract: Compared to $\text{Pb}(\text{Zr}_{1-x}\text{Ti}_x)\text{O}_3$ (PZT) polycrystalline ceramics, relaxor-PT single crystals offer significantly improved performance with extremely high electromechanical coupling and piezoelectric coefficients, making them promising materials for piezoelectric transducers, sensors and actuators. The recent advances in crystal growth and characterization of relaxor-PT-based ferroelectric single crystals are reviewed in this paper with emphases on the following topics: (1) the large crystal growth of binary and ternary relaxor-PT-based ferroelectric crystals for commercialization; (2) the composition segregation in the crystals grown from such a solid-solution system and possible solutions to reduce it; (3) the crystal growth from new binary and ternary compositions to expand the operating temperature and electric field; (4) the crystallographic orientation dependence and anisotropic behaviors of relaxor-PT-based ferroelectric crystals; and (5) the characterization of the dielectric, elastic and piezoelectric properties of the relaxor-PT-based ferroelectric crystals under small and large electric fields.

Keywords: relaxor-based ferroelectric crystals; composition segregation; anisotropic behavior; piezoelectric properties; dielectric properties

1. Introduction

The ferroelectric system, $\text{Pb}(\text{Zr}_{1-x}\text{Ti}_x)\text{O}_3$ (PZT), which was discovered 60 years ago [1], is playing an important role in modern transducer, sensor and actuator industries. PZT ceramics, with a composition lying near a morphotropic phase boundary (MPB) between the tetragonal and rhombohedral phases, exhibit anomalously high dielectric and piezoelectric properties as a result of enhanced polarizability arising from the coupling between two equivalent energy states, allowing optimum domain reorientation during the poling process [2–4]. After the discovery of PZT, searching for alternative MPB systems other than that found in PZT led to extensive studies of relaxor-based ferroelectrics and their solid solutions with PbTiO_3 (PT). A schematic ternary phase-diagram depicting MPBs in PZT and relaxor-PT systems is shown in Figure 1 [5]. Lead-based relaxor materials are complex perovskites with the general formula $\text{Pb}(\text{B}_\text{I}\text{B}_\text{II})\text{O}_3$ ($\text{B}_\text{I} = \text{Mg}^{2+}, \text{Zn}^{2+}, \text{Ni}^{2+}, \text{Sc}^{3+}, \text{Fe}^{3+}, \text{Yb}^{3+}, \text{In}^{3+}$, etc., $\text{B}_\text{II} = \text{Nb}^{5+}, \text{Ta}^{5+}, \text{W}^{6+}$, etc.), which characteristically show a broad and frequency dispersive dielectric maxima [4,6–8]. A variety of different relaxor-PT systems have been extensively studied in the form of single crystals [9–11]. Relaxor-PT single crystals, such as $\text{Pb}(\text{Zn}_{1/3}\text{Nb}_{2/3})\text{O}_3$ - PbTiO_3 (PZN-PT) and $\text{Pb}(\text{Mg}_{1/3}\text{Nb}_{2/3})\text{O}_3$ - PbTiO_3 (PMN-PT) have been found to offer significant high performance with electromechanical coupling (k_{33}) >90% and piezoelectric coefficients (d_{33}) > 1500 pC/N in contrast to PZT polycrystalline ceramics ($k_{33} \sim 75\%$, $d_{33} \sim 400$ –600 pC/N), making them promising candidates for medical and sonar transducers, industrial sensors and solid-state actuators, which need high sensitivity and a broad bandwidth [4,12–14]. In this paper, major advances in the crystal growth and characterization of relaxor-PT-based piezoelectric single crystals are reviewed with focuses on large-sized crystal growth process development and composition modification to improve the thermal and electrical stability of piezoelectric, dielectric and elastic properties.

Figure 1. Ternary phase-diagram depicting morphotropic phase boundaries (MPBs) in $\text{Pb}(\text{Zr}_{1-x}\text{Ti}_x)\text{O}_3$ (PZT) and relaxor-PT systems. Reprinted with permission from [5]. Copyright 1994 the Japan Society of Applied Physics.



2. Relaxor-PT-Based Ferroelectric Crystal Growth

2.1. PZN-PT and PMN-PT

It is always a great challenge to grow single crystals of complex compounds. The successful growth of PMN-PT and PZN-PT single crystals became a real breakthrough that started a new era in relaxor-PT-based ferroelectric crystal research. Binary PMN-PT and PZN-PT solid-solutions, which present a perovskite phase, can be synthesized from complex oxide systems of $\text{PbO-MgO(ZnO)-Nb}_2\text{O}_5\text{-TiO}_2$. However, the formation of the parasitic pyrochlore phase was the most problematic in the crystal growth process, causing instability in crystallization and generating defects and polycrystals [15,16]. Several other challenges to the growth of large single crystals include volatilization of PbO, the high melting point of the oxides and the composition segregation of the solid solutions [15,16].

PMN-PT and PZN-PT crystals were first grown by the flux method, which demonstrated ultrahigh piezoelectric coefficients and strain levels with low hysteresis [4,10]. The flux method is a type of high temperature solution growth, which is based on the spontaneous nucleation that occurs when supersaturation happens in a slow cooling process. The method has been broadly adopted in the growth of new crystal materials, especially those that melt incongruently or volatilize seriously before reaching melting temperature [17]. Difficulty in crystallization orientation control, slow growth rate, small crystal size and flux inclusions are common limitations of the flux growth method. To overcome these limitations, several improved high temperature solution growth methods, including top-seeded solution growth (TSSG) and solution-Bridgman growth, have been developed based on the basic flux method for the growth of PMN-PT and PZN-PT crystals [18,19]. In top-seeded solution growth, by introducing a perovskite seed crystal into the solution, it became possible to trigger single nucleation and control the crystallization orientation to obtain large-sized single crystals. The solution-Bridgman growth combines the flux growth and the vertical Bridgman growth, which is more suitable for growing large crystals. Currently, PMN-PT and PZN-PT single crystals grown by high temperature solution methods have reached the sizes of 35 mm in edge length or two inches in diameter.

The effective crystal growth technologies have been explored extensively after the extraordinary piezoelectric performance of PMN-PT and PZN-PT crystals were revealed. DTA study indicated that PMN-PT melts congruently [16,20,21], suggesting the possibility of growing PMN-PT crystals from the melt directly. These studies also showed that PMN-PT has a more stable perovskite phase and exhibits less of a tendency to form the parasitic pyrochlore phase compared to PZN-PT. By pre-synthesizing PMN-PT and using sealed Pt crucibles to prevent the volatilization of PbO at high temperature, PMN-PT single crystals have been grown directly from the melt using the Bridgman method [22,23]. Compared to flux growth, the Bridgman technique can grow large-sized single crystal boules along specific crystallographic orientations with a higher growth rate, which can potentially reduce the cost of PMN-PT crystals, to be competitive with the high quality piezoelectric ceramics used in high-end applications.

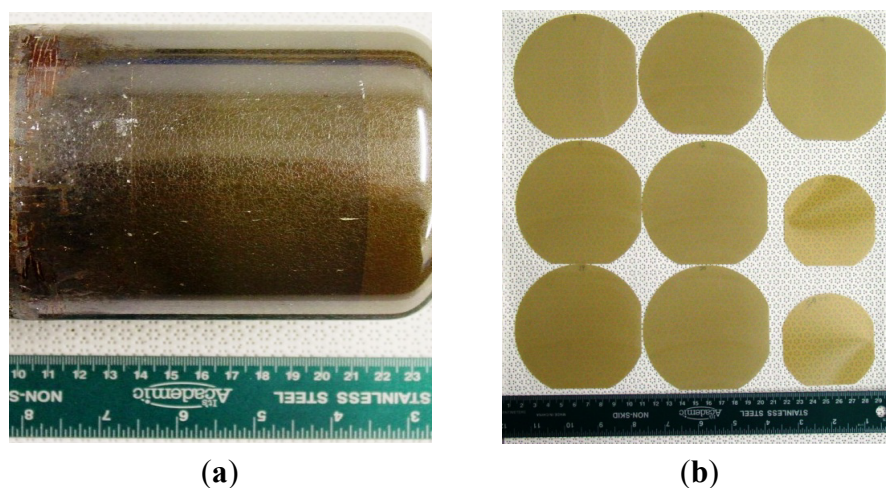
It was indicated that the formation of inclusions/voids, spontaneous nucleation, crystallization orientation control and reduction of the composition variation are the major challenges in the growth of large-sized and high quality PMN-PT crystals by the Bridgman process [15,16,22,23]. Owing to the

large difference in melting point and density between each oxide, especially between PbO ($T_m = 886\text{ }^{\circ}\text{C}$, $\rho = 9.53\text{ g/cm}^3$) and MgO ($T_m = 2852\text{ }^{\circ}\text{C}$, $\rho = 3.58\text{ g/cm}^3$), it is usually difficult to get a homogeneous perovskite phase by directly mixing the oxides without the presence of a minor amount of the pyrochlore phase [16]. Pre-synthesized PMN-PT using a modified columbite precursor method has been proven to be the most efficient way to eliminate the pyrochlore phase [24]. In this method, instead of using oxides, MgO and Nb₂O₅, columbite precursor, MgNb₂O₆, which has a similar structure to the perovskite phase, was synthesized by solid-state reaction and used as the raw material to bypass the intermediate pyrochlore phase reaction. The high-quality PMN-PT compound can also be synthesized by different routes, including the coprecipitation method [25] and the molten salt synthesis method [26]. The inclusions/voids formation, dendrite growth and polycrystal formation are all largely attributed to the pyrochlore phase formed in the raw material; however, such defects can be also induced by other factors, such as the non-stoichiometry of the raw material, impurities and too fast of a growth rate.

Since PMN-PT crystal exhibits the highest piezoelectric response along the $\langle 001 \rangle$ orientation, $\langle 001 \rangle$ -cut wafers have become highly demanded [16]. Owing to the inevitable axial composition segregation of this solid-solution in the Bridgman process [22,27], highly uniform (001) wafers can only be produced by successful and repeatable $\langle 001 \rangle$ -oriented crystal growth. However, since PMN-PT presents the slowest growth rate along the low-index $\langle 001 \rangle$ orientation ($R_{\langle 001 \rangle} < R_{\langle 110 \rangle} < R_{\langle 111 \rangle}$), the Bridgman growth of bulk PMN-PT crystal along $\langle 001 \rangle$ becomes the most challenging. Spontaneous nucleation is apt to happen and dominate the crystallization process, forming polycrystals instead of a single crystal. The growth process in Bridgman growth has to be finely controlled to avoid the spontaneous nucleation on the solid-liquid interface.

Significant progress has been made in the Bridgman growth of PMN-PT in recent years. High-quality and large-sized PMN-PT crystals without macro-defects have been successfully grown along different crystallographic orientations, including $\langle 001 \rangle$, $\langle 110 \rangle$ and $\langle 111 \rangle$. Currently, $\langle 001 \rangle$ -oriented PMN-PT crystals with a 100-mm diameter are commercially available. Figure 2 shows a 100-mm diameter crystal boule grown along $\langle 001 \rangle$ and the (001) wafers cut from it.

Figure 2. A 100-mm diameter Pb(Mg_{1/3}Nb_{2/3})O₃-PbTiO₃ (PMN-PT) crystal grown along $\langle 001 \rangle$ (a) and 100-mm diameter (001) wafers (in comparison with 75-mm diameter ones); (b) courtesy of TRS Technologies Inc., State College, PA, USA.



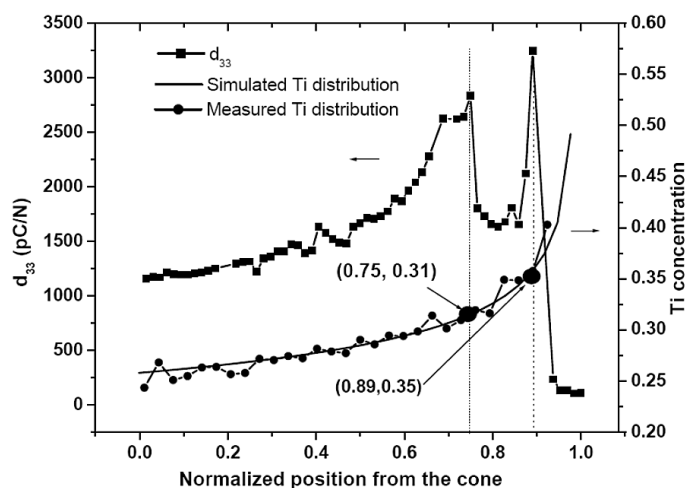
Although the Bridgman method is a very promising technique, the composition segregation issue has to be addressed. Since PMN-PT is a complete solid-solution system, as shown by its high temperature phase diagram, it inevitably exhibits an inhomogeneous composition distribution along crystal boules grown by the Bridgman method [22,27], resulting in the variation of dielectric and piezoelectric properties along the growth direction. Even though the composition variation along the growth direction can be restrained to some degree by applying a higher growth rate and a lower axial temperature gradient across the solid-liquid interface, it can never be eliminated due to the thermodynamic nature of the solid solution system [27]. The composition distribution can be simulated by a well-established equation used for describing the composition segregation behavior in solid solution systems during the normal solidification process [17]:

$$c_s = k_e c_0 (1 - g)^{k_e - 1} \quad (1)$$

Where k_e is the effective segregation coefficient, C_s and C_0 the solute concentration in the crystal and the starting melt and g the solidified fraction.

It was verified by chemical analysis that, except for Pb, all other elements in PMN-PT crystals exhibit composition segregation during crystal growth, with effective segregation coefficients of Nb and Mg larger than one, while that of Ti is smaller than one. Figure 3 compares the piezoelectric property (d_{33}) variation with the composition distributions measured by EPMA and simulated by the above equation [28], which shows the region between two peaks roughly corresponding to a PT (PbTiO_3) concentration of 31% to 35%, which is basically consistent with the broad MPB region between rhombohedral and tetragonal phases proposed by Guo *et al.* [29,30]. The simulated effective segregation coefficient of Ti in this run was around 0.83. Studies show that the mixed phases, including metastable ferroelectric monoclinic (FE_m) and ferroelectric orthorhombic (FE_o) phases, are possibly present in this region [29–31].

Figure 3. Comparison of piezoelectric property (d_{33}) variation with the composition distribution. Reprinted with permission from [28]. Copyright 2008 CRC Press.



As described above, the existence of the composition segregation-induced longitudinal property variation is one of the main disadvantages of Bridgman growth. Although the $\langle 001 \rangle$ -oriented Bridgman growth can produce desirable (001) wafers with very high lateral uniformity in each wafer, it cannot

eliminate the wafer-to-wafer variation. Usually, only a portion of each boule possesses the required PT composition range that meets the desired piezoelectric and dielectric properties. To further reduce or even eliminate the composition segregation in PMN-PT crystals, several innovative crystal growth methods were proposed, including, zone leveling [16], continuous feeding Bridgman growth [32] and solid-state crystal growth [28,33].

Zone leveling, a type of zone-melting crystal growth method, has been developed to produce a uniform, or level, distribution of solute in polycrystals and single crystals in many applications [34], which was proposed as an alternative method to prevent composition segregation in PMN-PT crystal growth [16]. Theoretically, zone leveling can produce a flat composition distribution except for the initial and last frozen regions (zones). The zone melting growth of PMN-PT crystals was conducted in both RF induction heated and resistance heated furnaces [27,28]. Constant composition at PT = 32% was observed over ~60 mm of total boule length (~80 mm) in a zone-leveled boule compared with the constantly changing composition usually observed in Bridgman grown crystals [27].

As proposed, continuous feeding Bridgman is a modified Bridgman method, in which PMN powder or pellets are charged slowly into the melt during crystal growth to keep the concentration of Mg, Nb and Ti constant. The challenge of this method is to minimize the thermal disturbance to the melt, as well as to prevent PbO from evaporation during the feeding operation. This technique was demonstrated successfully by the growth of 80-mm diameter PMN-PT crystals [35]. Curie temperature (T_C) was controlled to a range of 130–138 °C in a 116-mm-long portion of such a crystal, which is much narrower than that in the crystals grown by the regular Bridgman technique (usually 120–160 °C). As T_C is strongly correlated to the composition, it is indicated that the crystal possesses a much narrower composition distribution along the length.

Solid-state crystal growth (SSCG) is based on an abnormal grain growth in the sintering of polycrystalline ceramics, in which a small number of grains is grow quickly by consuming surrounding fine matrix grains [28]. In SSCG of a PMN-PT crystal, a small BZT ($\text{Ba}(\text{Zr}_{0.1}\text{Ti}_{0.9})\text{O}_3$) single crystal is used as a seed to control the nucleation of abnormal grains, so that a large single crystal can be obtained in the polycrystalline matrix. Since the polycrystalline ceramic matrix is not melted, the composition segregation does not happen. The other advantages that the SSCG method provides include low process temperature, no need for Pt crucibles and crystal growth of incongruently melting compositions. However, in this process, it is hard to completely eliminate the porosity in the crystals, which may affect the mechanical and optical properties [33]. Currently, PMN-PT crystals larger than $50 \times 50 \times 10 \text{ mm}^3$ can be produced by the SSCG method [28].

2.2. High T_C Relaxor-PT Binary Crystals

Even though large-sized and high-quality PMN-PT crystals can be grown directly from the melt, their low ferroelectric-to-ferroelectric phase transition temperatures and low coercive field restrict their applications largely. The piezoelectric/dielectric properties of rhombohedral-phase PMN-PT crystals have a strong temperature dependence. For instance, PMN-29%PT exhibit a 52% change in the dielectric constant from room temperature to 55 °C. This change negatively affects the transducer impedance and matching circuitry and, therefore, the power delivery system. Furthermore, the rhombohedral-to-tetragonal ferroelectric phase transition temperature (T_{rt}) for PMN-PT crystals with

near MPB compositions is as low as 85 °C to 95 °C, which becomes the maximum applicable temperature. In addition to the temperature stability, PMN-PT crystals have a coercive field as low as 2–2.5 kV/cm, limiting the amplitude of the driving field and the power output. High Curie temperature piezoelectric crystals are desired to expand the operational temperature and electric field, to reduce the properties' temperature dependence and to increase the acoustic power output [36].

Table 1 lists broadly investigated binary relaxor-PT systems, among which the $\text{Pb}(\text{Sc}_{1/2}\text{Nb}_{1/2})\text{O}_3$ - PbTiO_3 (PSN-PT), $\text{Pb}(\text{In}_{1/2}\text{Nb}_{1/2})\text{O}_3$ - PbTiO_3 (PIN-PT) and $\text{Pb}(\text{Yb}_{1/2}\text{Nb}_{1/2})\text{O}_3$ - PbTiO_3 (PYN-PT) were found to possess relatively high Curie temperatures near their MPB compositions [5,37,38]. Henceforth, numerous research has focused on these binary systems in single crystal form in order to achieve high performance over a wide temperature range [24,39–50].

Table 1. Morphotropic phase boundaries in perovskite $\text{Pb}(\text{B}_\text{I}\text{B}_\text{II})\text{O}_3$ -PT ceramic systems.

Binary System	PT (x) at MPB	T_C (°C) at MPB	T_{R-T} (°C) at MPB
$(1-x)\text{Pb}(\text{Zn}_{1/3}\text{Nb}_{2/3})\text{O}_3$ - $x\text{PbTiO}_3$ (PZN-PT)	~0.09	~180	95
$(1-x)\text{Pb}(\text{Mg}_{1/3}\text{Nb}_{2/3})\text{O}_3$ - $x\text{PbTiO}_3$ (PMN-PT)	~0.33	~150	80
$(1-x)\text{Pb}(\text{Ni}_{1/3}\text{Nb}_{2/3})\text{O}_3$ - $x\text{PbTiO}_3$ (PNN-PT)	~0.40	~130	—
$(1-x)\text{Pb}(\text{Co}_{1/3}\text{Nb}_{2/3})\text{O}_3$ - $x\text{PbTiO}_3$ (PCN-PT)	~0.38	~250	—
$(1-x)\text{Pb}(\text{Sc}_{1/2}\text{Nb}_{1/2})\text{O}_3$ - $x\text{PbTiO}_3$ (PSN-PT)	~0.43	~260	100
$(1-x)\text{Pb}(\text{Sc}_{1/2}\text{Ta}_{1/2})\text{O}_3$ - $x\text{PbTiO}_3$ (PST-PT)	~0.45	~205	—
$(1-x)\text{Pb}(\text{Fe}_{1/2}\text{Nb}_{1/2})\text{O}_3$ - $x\text{PbTiO}_3$ (PFN-PT)	~0.07	~140	—
$(1-x)\text{Pb}(\text{In}_{1/2}\text{Nb}_{1/2})\text{O}_3$ - $x\text{PbTiO}_3$ (PIN-PT)	~0.37	~320	120
$(1-x)\text{Pb}(\text{Yb}_{1/2}\text{Nb}_{1/2})\text{O}_3$ - $x\text{PbTiO}_3$ (PYN-PT)	~0.50	~360	160
$(1-x)\text{Pb}(\text{Mg}_{1/2}\text{W}_{1/2})\text{O}_3$ - $x\text{PbTiO}_3$ (PMW-PT)	~0.55	~60	—
$(1-x)\text{Pb}(\text{Co}_{1/2}\text{W}_{1/2})\text{O}_3$ - $x\text{PbTiO}_3$ (PCW-PT)	~0.45	~310	—

PSN-PT single crystals with MPB compositions were successfully grown by the flux method using PbO - B_2O_3 as the flux [39–41]. The growth temperature range and B_2O_3 ratio in the flux are deemed very important because of the perovskite stability. The perovskite crystal size obtained was found to be 2–15 mm in length. PSN-33%PT crystals were reported to possess a high Curie temperature, $T_C \sim 206$ °C (30–50 °C higher than PMN-PT and PZN-PT systems), while the electromechanical coupling factor (k_{33}) and dielectric constant were found to be only 72% and 960, respectively.

Single crystals of PIN-PT and their electromechanical properties were also studied. It was reported that PIN-28PT crystals could be grown using the flux method with PbO - PbF_2 - B_2O_3 . The obtained crystals were $20 \times 10 \times 5$ mm³ in size, which is much larger compared to PSN-PT crystals [42]. The Curie temperature was reported to be 260 °C with a rhombohedral-to-tetragonal phase transition temperature, T_{rt} , around 100 °C. The electromechanical coupling in the longitudinal mode (k_{33}) was estimated to be 85% at room temperature [42]. The same research group also reported growing PIN-PT crystals by the solution Bridgman method using PbO - B_2O_3 as the flux, in which a crystal with 10 mm in diameter and 10 mm in length was obtained and the growth direction was determined along the [110] direction. The T_C and T_{rt} were found to be 300 °C and 120 °C, respectively, for PIN-31%PT crystals [43]. It was also reported the PIN-34%PT crystals were grown by using PMNT31 as a seed crystal. The obtained crystals were found to have high piezoelectric coefficients $d_{33} \sim 2000$ pC/N and

electromechanical coupling k_{33} of about 94%, comparable to the PMN-PT system, while exhibiting higher T_C at 200 °C [44].

For the systems mentioned above, T_C on the order of 200–300 °C has been found; however, T_{rt} is still in the range of only 70–120 °C. PYN-PT with MPB composition was found to possess the highest T_C of about 360 °C among all of the lead-based relaxor-PT systems, similar to the commercial PZT5A ceramics. Piezoelectric single crystals in the PYN-PT system were grown using the flux method with Pb_3O_4 or Pb_3O_4/B_2O_3 as the flux. Perovskite PYN-PT solid solutions were prepared using the “wolframite process”, which consists of the synthesized B-site precursor, $YbNbO_4$, prior to reaction with PbO and TiO_2 [24,45,46]. The obtained crystals were light yellow in color and 2–8 mm in size.

Table 2 summarized the detailed dielectric and piezoelectric properties of different relaxor-PT single crystal systems, in which it can be seen that all of the single crystals possess high electromechanical coupling, except for PSN-PT. The dielectric and piezoelectric properties were found to not only depend on the composition, but also depend on the Curie temperature: the higher Curie temperature the crystal system possesses, the lower dielectric constant and piezoelectric properties were observed; however, higher coercive fields were found with higher T_C .

Table 2. Detailed dielectric and piezoelectric properties of relaxor-PT single crystals.

Crystal	T_C (°C)	T_{R-T} (°C)	E_c (kV/cm)	K_{33}^T	d_{33} (pC/N)	k_{33}	Reference
PMN-31PT	143	90	2.5	5100	2000	90%	[47]
PZN-4.5PT	155	120	3.2	4400	2100	90%–91%	[47]
PZN-8PT	170	100	4	6000	2500	93%	[47]
PZN-12PT	190	–	8.5	870	576	86%	[48]
PSN-33PT	206	–	6	960	–	72%	[39]
PIN-28PT	260	100	18	1500	700	85%	[42,49]
PIN-34PT	200	<100	–	5000	2000	94%	[44]
PYN-40PT	270	168	10	2700	1200	88%	[47]
PYN-45PT	325	160	12.5	2000	2000	88%–90%	[46]
BS-57PT	402	349	13.7	3000	1150	91%	[50]

2.3. High T_C PMN-PT-Based Ternary Crystals

As described above, all of the binary relaxor-PT single crystals that have a Curie temperature higher than that of PMN-PT single crystals could only be grown by the flux method. Owing to the instability of the perovskite phase of these binary compositions, commercialization of these high T_C crystals was hindered by the availability of large-sized crystals. Recently, it was demonstrated that, by adding PMN-PT into some of the high T_C binary systems, the formed PMN-PT-based ternary compositions could have a relatively stable perovskite phase, offering the possibility to grow large crystals with a pure perovskite phase [51,52].

Among the broadly studied ternary systems, substantial progress has been made on the growth of large-sized PIN-PMN-PT crystals by the Bridgman process. For the preparation of PIN-PMN-PT, both a wolframite precursor, $InNbO_4$, and a columbite precursor, $MgNb_2O_6$, were firstly synthesized, respectively, by calcination of oxides at 1000–1200 °C. Using these precursors, PIN-PMN-PT with a pure perovskite phase was synthesized by another calcination process at lower temperature (750–900 °C).

Like PMN-PT crystals, PIN-PMN-PT crystals with a pure perovskite phase form during solidification, so the crystals can be grown directly from the melt by the Bridgman process. By presenting a seed crystal, PIN-PMN-PT crystals with a diameter up to 75 mm have been grown along the preferred crystallographic orientations, including $\langle 001 \rangle$, $\langle 110 \rangle$ and $\langle 111 \rangle$. Figure 4 shows the as-grown PIN-PMN-PT crystals. It was found that the T_{rt} and T_{C} of PIN-PMN-PT (26%–36%PIN) crystals reach 120–140 °C and 160–200 °C, respectively, marking a 35–40 °C increase compared to PMN-PT crystals with a similar PT concentration. Furthermore, they exhibit a similar d_{33} value (1100–2200 pC/N) as PMN-PT crystals, but a much higher coercive field (4.5–6 kV/cm).

Figure 4. Seventy five-millimeter and 50-mm diameter $\langle 001 \rangle$ -oriented PIN-PMN-PT crystals grown by the Bridgman process (courtesy of TRS Technologies, Inc., State College, PA, USA).



PZT ceramics have been the mainstay for high-performance piezoelectric applications. However, the attempt to grow single-crystal PZT has not been successful. So far, only very small crystals of PZT can be produced by high temperature solution growth, which cannot provide samples for complete property measurement. As PMN-PT crystals, chemically homogeneous PMN-PZT crystals were also successfully grown by the solid-state crystal growth (SSCG) process [53]. By this delicately controlled sintering process, the as-grown PMN-PZT crystals achieved a similar size and quality as SSCG-grown PMN-PT crystals. Interestingly, the T_{C} of all PMN-PZT crystals is approximately 200 °C; however, by changing the PMN/PZ/PT ratio, T_{rt} could be adjusted in the range of 100–160 °C, while d_{33} in the range of 1000–2000 pC/N [53].

Recently, some other PMN-PT-based ternary solid solution systems, including $\text{Pb}(\text{Yb}_{1/2}\text{Nb}_{1/2})\text{O}_3$ - $\text{Pb}(\text{Mg}_{1/3}\text{Nb}_{2/3})\text{O}_3$ - PbTiO_3 (PYN-PMN-PT), $\text{Pb}(\text{In}_{1/2}\text{Nb}_{1/2})\text{O}_3$ - $\text{Pb}(\text{Zn}_{1/3}\text{Nb}_{2/3})\text{O}_3$ - PbTiO_3 (PIN-PZN-PT) and $\text{Pb}(\text{Fe}_{1/2}\text{Nb}_{1/2})\text{O}_3$ - $\text{Pb}(\text{Yb}_{1/2}\text{Nb}_{1/2})\text{O}_3$ - PbTiO_3 (PFN-PYN-PT), have been investigated [54–57]. By the top-seeded solution growth (TSSG) method, crystals with compositions near an MPB have been grown, which show comparable piezoelectric properties to PMN-PT crystals, but higher Curie temperature and/or coercive field. As the TSSG method has been successfully applied to the large-scale production of some nonlinear optical crystals, such as β - BaBO_4 (BBO) and KTiOPO_4 (KTP) crystals, it is possible that it can be tailored to produce large crystals of these ternary solid solution crystals. Currently, PYN-PMN-PT crystals with a length and width over 3 cm have been obtained by the TSSG method. As complex flux systems are required to facilitate crystallization and to achieve a high crystal growth rate, the main challenge in the TSSG growth of crystals of these complex ternary compositions is to repeatedly produce high quality crystals that maintain consistent properties.

Table 3 summarizes the major piezoelectric and dielectric properties of PMN-PT-based ternary solid solution crystals that can operate at higher temperature and a higher electric field than current state-of-the-art PMN-PT single crystals.

Table 3. Detailed dielectric and piezoelectric properties of PMN-PT-based ternary crystals.

Crystal	T_c (°C)	T_{R-T} (°C)	E_c (kV/cm)	K_{33}^T	d_{33} (pC/N)	k_{33}	Reference
PMN-29PT	135	96	2	5400	1540	91%	[58]
PMN-31PT	143	90	2.5	5100	2000	90%	[47]
PIN-PMN-PT *	160~200	120~140	4.5~6	4000~5000	1100~2200	89%~93%	[59]
PMN-PZT **	190~200	100~160	>5	3000~6000	1000~2000	89%~92%	[53]
20PYN-40PMN-40PT	180	130	5.4	2400	2440~2580	90.9%	[54]
15PYN-53PMN-32PT	205	50	7	6270	1800	90%	[55]
30PIN-33PbZN-37PT	236	175	14.3	2500	1900~2100	86%	[56]
10PFN-38PYN-52PT	325	155	10.3	1620	1100	70%	[57]

* 26%~36% PIN and 28%~32% PT; ** Composition PMN-PZT-11~PMN-PZT-5.

3. Relaxor-Based Ferroelectrics Crystal Characterization

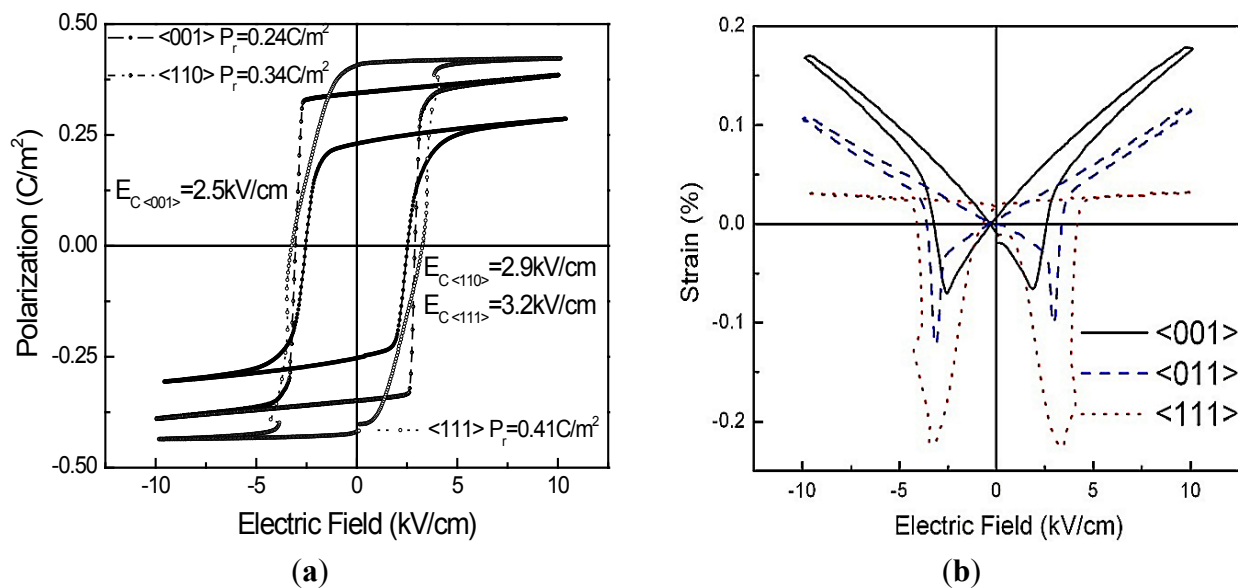
3.1. Crystallographic Orientation Dependence of Property

It was reported that the relaxor-PT single crystals show a strong anisotropic behavior. Thus, in this section, the dielectric, ferroelectric, piezoelectric and electromechanical properties were studied as a function of their main crystallographic orientations, *i.e.*, along the $\langle 001 \rangle$, $\langle 110 \rangle$ and $\langle 111 \rangle$ directions. As reported, for rhombohedral relaxor-PT single crystals, different engineered domain configurations can be obtained by poling along different crystallographic directions. Since the spontaneous polarization is along the $\langle 111 \rangle$ crystallographic direction, a single domain can be achieved when the crystal was poled along $\langle 111 \rangle$, and the obtained domain configuration was 1R, while the engineered domain configurations can be labeled as 4R and 2R, when polarized along the $\langle 001 \rangle$ and $\langle 110 \rangle$ directions, respectively [60].

Figure 5 shows the measured electric field-induced polarization (a) and strain (b) hysteresis loops for $\langle 001 \rangle$ -, $\langle 110 \rangle$ - and $\langle 111 \rangle$ -oriented PMN-30% PT crystals. The remnant polarization, P_r , and coercive field, E_c , were found to be dependent on the orientation. From the symmetric loops, the P_r was found to be on the order of 0.24 C/m², 0.34 C/m² and 0.41 C/m² for the $\langle 001 \rangle$, $\langle 110 \rangle$ and $\langle 111 \rangle$ orientations, while the coercive field, E_c , was on the order of 2.5 kV/cm, 2.9 kV/cm and 3.2 kV/cm, respectively. It is known that there are eight possible polarization orientations along the pseudo-cubic $\langle 111 \rangle$ direction for rhombohedral relaxor-PT single crystals (3-m symmetry). Upon applying an electric field, the dipoles reorientate as close as possible to the applied electric field direction. For $\langle 001 \rangle$ -poled crystals, there are four equivalent polar vectors along the $\langle 111 \rangle$ direction, with an inclined angle of -54.7° from the poling field. The four $\langle 111 \rangle$ domains are equivalent, with a domain-engineered configuration resulting in a macro symmetry of 4mm. For $\langle 110 \rangle$ -poled crystals, there are two equivalent polar vectors along the $\langle 111 \rangle$ direction, which will rotate 35.5° toward the applied field direction of $\langle 110 \rangle$ with a designated domain-engineered configuration of 2R. For this case, the macroscopic symmetry is in mm². In contrast, there is only one polar vector along the $\langle 111 \rangle$

direction for $\langle 111 \rangle$ -poled ferroelectric crystals; thus, it will form a monodomain state, 1R, exhibiting a symmetry of 3m. According to the domain-engineered configurations, the polarization level derived from the hysteresis loops should correspond, in theory, to the intrinsic value along the polar axis of the monodomain crystal, P_s , following $P_{r\langle 001 \rangle} = P_{r\langle 110 \rangle}/\sqrt{2} = P_{r\langle 111 \rangle}/\sqrt{3}$ [61–63]. As expected, the P_r values for the different orientations obtained from Figure 5a corresponded well to the predicted values. From Figure 5b, it is seen that in the sequence of orientation, $\langle 001 \rangle$, $\langle 011 \rangle$ and $\langle 111 \rangle$, the electric field required to reverse the domain (coercive field E_C) increased, which is consistent with that indicated by the polarization hysteresis, while the positive strain achieved after the domain reorientation decreased.

Figure 5. Polarization hysteresis for PMN-30% PT crystals along crystallographic orientations $\langle 001 \rangle$, $\langle 110 \rangle$ and $\langle 111 \rangle$. Reprinted with permission from [61]. Copyright 2009 AIP Publishing.



Analogous to dielectric and ferroelectric properties, the piezoelectric and electromechanical properties were also found to show anisotropic behaviors. The longitudinal piezoelectric coefficient, d_{33} , was found to reach its peak value when poled along crystallographic direction $\langle 001 \rangle$, while it drops significantly when poled along the $\langle 111 \rangle$ orientation. The transverse piezoelectric response for relaxor-PT perovskite crystals is more complicated, where it has been reported that there are four different vibration modes showing good piezoelectric characteristics. These modes are $(001)/\langle 100 \rangle$, $(001)/\langle 110 \rangle$, $(110)/\langle 001 \rangle$ and $(110)/\langle \bar{1}10 \rangle$, where the first number indicates the electrode face (perpendicular to poling direction) and the second number is the acoustic wave propagation direction [64]. It has been demonstrated that the highest transverse piezoelectric coefficients are obtained from crystals poled along $\langle 110 \rangle$ and vibrated along the $\langle 001 \rangle$ direction [64–68], with small signal d_{32} coefficients on the order of $\sim 1500 \text{ pC/N}$ and electromechanical coupling factor $k_{32} \sim 0.90$ in PZN-PT, PMN-PT and PMN-PZT crystals.

The main properties for longitudinal and transverse modes for PIN-PMN-PT single crystals at room temperature are listed in Table 4 [69]. The dielectric permittivity was found to be on the order of 4400, 3400 and 700 for $\langle 001 \rangle$ -, $\langle 110 \rangle$ - and $\langle 111 \rangle$ -poled rhombohedral PIN-PMN-PT crystals, respectively,

while the dielectric losses were 0.2% and 0.1%, respectively. The longitudinal electromechanical coupling factor, k_{33} , was found to be 0.92 for $\langle 001 \rangle$ samples, slightly higher than that of $\langle 110 \rangle$ -poled crystals (~ 0.91), but to drop significantly for $\langle 111 \rangle$ samples, being on the order of 0.43. The piezoelectric d_{33} was on the order of 1500 pC/N for the $\langle 001 \rangle$ cut, higher than the value for the $\langle 110 \rangle$ -oriented sample ~ 925 pC/N, while the d_{33} was found to be only ~ 90 pC/N for the $\langle 111 \rangle$ single-domain PIN-PMN-PT crystals, as observed in other relaxor-PT systems. The typical extensional transverse modes for the perovskite ferroelectric crystal were summarized in Table 4, as well, where the first number indicates the poling direction and the second number gives the vibration orientation. Unlike $\langle 001 \rangle$ -poled samples, a large discrepancy between the piezoelectric d_{31} and d_{32} was observed in $\langle 110 \rangle$ -poled crystals. The optimal transverse properties were found for (110)/ $\langle 001 \rangle$ cut (polarized along $\langle 110 \rangle$ with vibration along the $\langle 001 \rangle$ direction), with electromechanical coupling factor k_{32} on the order of 0.91 and corresponding piezoelectric d_{32} on the order of -1420 pC/N.

Table 4. Longitudinal and transverse piezoelectric and electromechanical properties for $\langle 001 \rangle$ -, $\langle 110 \rangle$ - and $\langle 111 \rangle$ -poled PIN-PMN-PT crystals.

PIN-PMN-PT			K_{ij}	loss	k_{ij}	d_{ij} (pC/N)	s_{ij}^E (pm ² /N)
Longitudinal	$ij = 33$	001	4400	0.2%	0.92	1500	68.0
		110	3400	0.1%	0.91	925	34.8
		111	700	0.1%	0.43	90	7.0
Lateral	$ij = 31$	001/100	4400	0.2%	0.50	-700	51.2
	$ij = 31$ (45°)	001/110	4400	0.2%	0.81	-800	25.0
	$ij = 32$	110/001	3400	0.1%	0.91	-1420	83.1
	$ij = 31$	110/ $\bar{1}10$	3400	0.1%	0.74	590	21.5

The temperature-dependent piezoelectric and electromechanical coupling for the above-mentioned modes are shown in Figures 6 and 7. Figure 6 presents the temperature-dependent characteristics of the longitudinal electromechanical coupling and piezoelectric coefficient for $\langle 001 \rangle$ - and $\langle 110 \rangle$ -poled PIN-PMN-PT crystals. The k_{33} for $\langle 001 \rangle$ -poled crystals was found to be on the order of 0.91 at -50°C , increasing to 0.94 at 125°C , the ferroelectric phase transition temperature, above which, the k_{33} decreased to only 0.78. In contrast, the coupling for the $\langle 110 \rangle$ -poled crystals was >0.90 at -50°C , slightly increased to 0.93 at a temperature of 116°C , above which, k_{33} dropped due to the rhombohedral-to-orthorhombic (R-O) phase transition. The orthorhombic-to-tetragonal (O-T) phase transition at 130°C was also observed in the coupling measurement. The piezoelectric coefficient, d_{33} , followed a similar trend as found in the dielectric behavior, reaching its peak value at the ferroelectric phase transition temperatures.

Figure 7 gives the temperature-dependent behavior of the transverse electromechanical coupling and piezoelectric coefficient for $\langle 001 \rangle$ - and $\langle 110 \rangle$ -poled samples along different vibration directions. It was found that the electromechanical coupling factors, k_{ij} , for different poling and vibration directions followed a similar tendency, maintaining their values in the temperature range from -50°C to T_{F-F} (ferroelectric phase transition temperature). The coupling factors were found to drop sharply above the phase transition temperature, where the crystals transformed to the tetragonal and/or orthorhombic phases. The piezoelectric coefficients, d_{31} and d_{32} (considering the symmetry of mm^2 in $\langle 110 \rangle$ -poled crystal, the value of d_{31} is assumed to be positive, while d_{32} is negative, based on IEEE

standards), showed a similar temperature-dependent behavior as found for the longitudinal mode, reaching peak values close to the ferroelectric transition temperature, above which, the transverse piezoelectric response disappeared.

Figure 6. Longitudinal electromechanical coupling k_{33} (a) and piezoelectric coefficient d_{33} (b) as a function of temperature for <001>- and <110>-poled single crystals. Reprinted with permission from [69]. Copyright 2009 AIP Publishing.

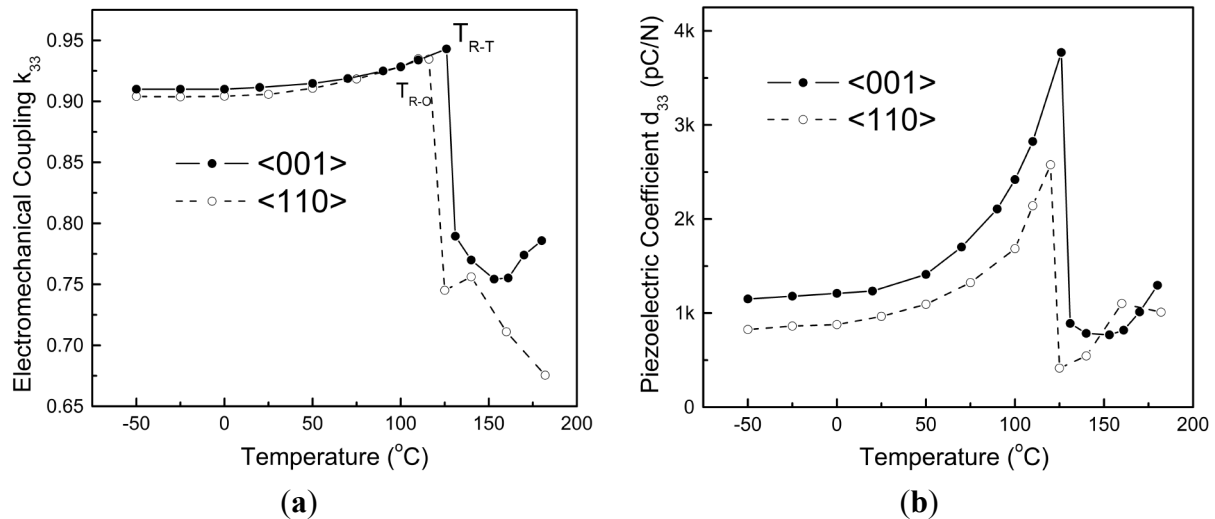
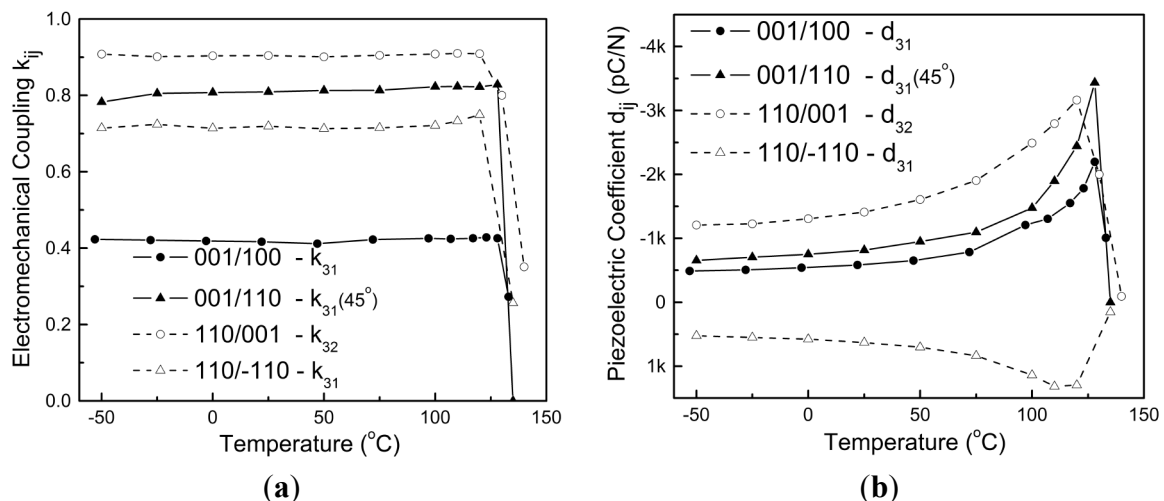


Figure 7. Transverse electromechanical coupling k_{31}/k_{32} and piezoelectric d_{31}/d_{32} as a function of temperature for <001>- and <110>-poled crystals. Reprinted with permission from [69]. Copyright 2009 AIP Publishing.



3.2. Full Sets of Electromechanical Properties (under a Low Electric Field)

For transducer and actuator modeling, it is very useful to obtain complete sets of electromechanical coefficients of relaxor-PT-based binary and ternary crystals. Two approaches were generally employed for such measurements. The first is the resonance method described in the IEEE standards [70]. Based upon the macro symmetries established by the domain-engineered configurations in rhombohedral relaxor-PT crystals, different sets of samples need to be prepared for the resonance measurements. For

the lower symmetry, more samples with different orientations need to be prepared, because there are more independent physical constants that exist. Furthermore, the resonance method requires the samples to have a large aspect ratio in order to avoid mode interference. However, the resonance method is relatively simple, since all of the measurements can be done on an impedance analyzer, and the calculated coefficients can be verified by different sets of equations. The other approach is the ultrasonic method, which is performed under a non-resonance condition and, therefore, may be more accurate than the resonance method, since there is no interference among different modes. By sending longitudinal and sheer waves into crystal samples with specific orientations, all material constants can be obtained. The samples required a pair of perfectly aligned faces, but no specific aspect ratio. However, large errors may emerge for the crystals with low symmetry when deriving constants from some mixed modes. To measure and derive a complete set of electromechanical coefficients for crystals with low symmetry, it may be necessary to combine the ultrasonic and resonance methods (a hybrid method) [71].

Table 5. Elastic compliance constants, s_{ij} (10^{-12} m²/N), and elastic stiffness constants, c_{ij} (10^{10} N/m²).

Properties	s_{11}^E	s_{12}^E	s_{13}^E	s_{33}^E	s_{44}^E	s_{66}^E
PMN-PT	52.1	−24.6	−26.4	59.9	16.0	28.3
PIN-PMN-PT	49.0	−20.0	−26.5	57.3	15.2	39.4
Mn:PIN-PMN-PT	45.4	−15.9	−28.1	62.4	15.4	27.8
Properties	s_{11}^D	s_{12}^D	s_{13}^D	s_{33}^D	s_{44}^D	s_{66}^D
PMN-PT	41.8	−34.8	−3.9	10.3	14.0	28.3
PIN-PMN-PT	38.2	−30.8	−4.0	10.3	14.3	39.4
Mn:PIN-PMN-PT	34.4	−26.9	−3.9	9.2	13.9	27.8
Properties	c_{11}^E	c_{12}^E	c_{13}^E	c_{33}^E	c_{44}^E	c_{66}^E
PMN-PT	12.4	11.1	10.4	10.8	6.3	3.5
PIN-PMN-PT	11.9	10.5	10.4	11.4	6.6	2.5
Mn:PIN-PMN-PT	12.8	11.1	10.8	11.3	6.5	3.6
Properties	c_{11}^D	c_{12}^D	c_{13}^D	c_{33}^D	c_{44}^D	c_{66}^D
PMN-PT	12.6	11.3	9.3	16.8	7.1	3.5
PIN-PMN-PT	12.3	10.9	9.0	16.7	7.0	2.5
Mn:PIN-PMN-PT	13.3	11.7	9.0	17.0	7.2	3.6

Relaxor-PT-based binary and ternary single crystals with near MPB compositions usually possess a rhombohedral phase with 3-m symmetry at a temperature lower than its rhombohedral-to-tetragonal phase transition temperature. However, when the crystals are poled along the pseudocubic [001] direction, it can be deemed as 4-mm symmetry macroscopically. The resonance method can be used to determine all of its independent electromechanical constants: six elastic, three piezoelectric and two dielectric constants. Such complete sets of constants of [001]-poled rhombohedral PMN-PT, PIN-PMN-PT and Mn:PMN-PIN-PT are listed in Tables 5–7 for comparison [72,73]. For the [011]-poled crystals (macroscopic mm²-symmetry), there are totally 17 independent electromechanical coefficients, nine elastic, five piezoelectric and three dielectric, to be determined. Either a resonance or a hybrid method

was employed to collect the full sets of properties for [011]-poled crystals [74–76]. For the [111]-poled crystals (macroscopic 3-m symmetry), a hybrid method was usually required [77].

Table 6. Piezoelectric coefficients, d_{ij} (pC/N), e_{ij} (C/m²), g_{ij} (10^{−3} Vm/N) and h_{ij} (10⁸ V/m).

Properties	d_{33}	d_{31}	d_{15}	e_{33}	e_{31}	e_{15}
PMN-PT	1540	−699	164	22.3	−3.9	10.3
PIN-PMN-PT	1320	−634	105	18.6	−4.8	6.9
Mn:PIN-PMN-PT	1341	−609	133	16.8	−5.2	8.6
Properties	g_{33}	g_{31}	g_{15}	h_{33}	h_{31}	h_{15}
PMN-PT	31.8	−15.4	9.9	26.2	−8.4	7.0
PIN-PMN-PT	35.6	−17.0	8.8	28.9	−7.4	6.5
Mn:PIN-PMN-PT	39.7	−18.1	11.3	34.2	−10.7	8.3

Table 7. Electromechanical coupling factors, k_{ij} , and dielectric constants, ϵ_{ij} (ϵ_0).

Properties	k_{33}	k_{31}	k_{15}	k_t	k_{31} (45 °C)
PMN-PT	0.89	0.44	0.27	0.56	0.77
PIN-PMN-PT	0.91	0.47	0.25	0.57	0.80
Mn: PIN-PMN-PT	0.92	0.49	0.31	0.58	0.80
Properties	ϵ_{33}^T	ϵ_{11}^T	ϵ_{33}^S	ϵ_{11}^S	
PMN-PT	5400	1560	910	1340	—
PIN-PMN-PT	4200	1335	729	1200	
Mn: PIN-PMN-PT	3811	1326	553	1169	

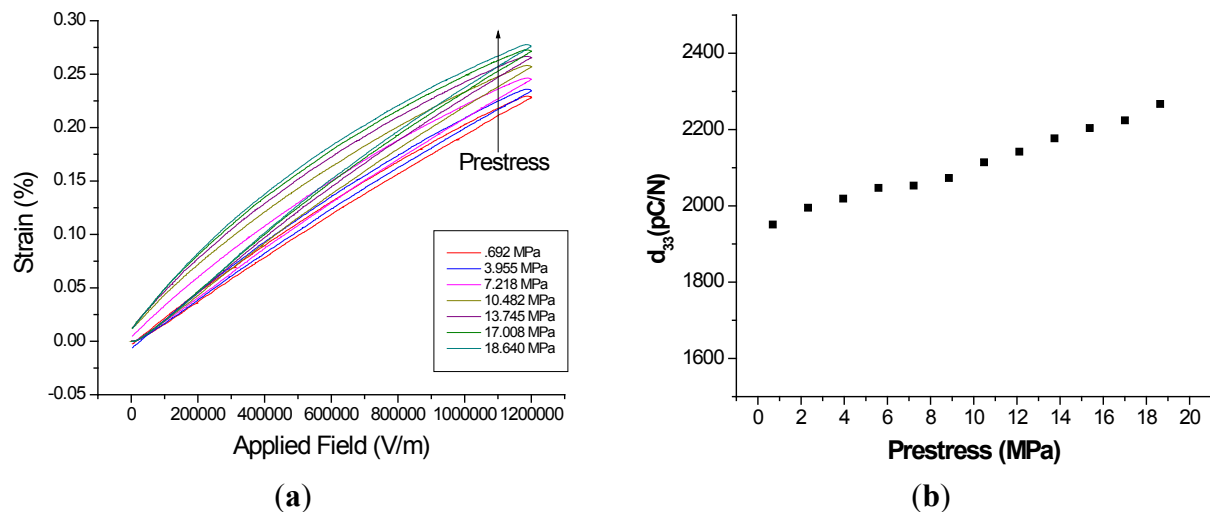
3.3. Characterization under a High Electric Field and High Mechanical Pressure

High-power underwater transducers and high-intensity focused ultrasound (HIFU) transducers may be driven under a large electric field and operated under high mechanical prestress [78,79]. These systems are operated over a short time duration; however, a very high source level and bandwidth may be required. To prevent the piezoelectric materials from going into a tensile state under the application of a high driving electric field, it is common practice to prestress the piezoelectric elements by employing a compressive uniaxial prestress upon them. However, the material property may change under the high mechanical prestress, due to the nonlinear effects of the ferroelectric materials. It is therefore important to determine not only the small signal characteristics, but also whether the materials maintain the bandwidth and linear performance under a high driving field and a prestress condition. In recent years, more studies have been done on relaxor-PT crystals, including PMN-PT, pure and Mn-doped PIN-PMN-PT crystals, under a combination of static compressive stress and high electric field [80–86]. The performance of relaxor-PT crystals under dynamic compressive stress has also been evaluated, but only under a small electric field [87,88].

The <001>-poled relaxor-PT crystals possess extremely high k_{33} and d_{33} , so the longitudinal extension mode is very attractive for high power transducer design. Figure 8 shows the strain-electric field (S-E) loops and extracted d_{33} measured under the unipolar electric field with constant amplitude (± 12 kV/cm)/frequency (1 Hz) when compressive prestress was applied to manganese (Mn)-doped rhombohedral PIN-PMN-PT crystal sample along the poling direction (<001>). It is indicated that the

crystal sample produced higher strain under higher uniaxial pressure with the cost of increased nonlinear loss (as suggested by the area of the strain-field hysteresis loops).

Figure 8. The strain-electric field (S-E) loops (a) and extracted d_{33} vs. prestress (b) under a unipolar electric field (Mn:PIN-PMN-PT crystal in the rhombohedral phase).



In high power transducer design, bipolar electric field (AC field) is often applied to drive the piezoelectric elements in the transducers, so it is necessary to evaluate the stability of the relaxor-PT crystals under uniaxial stress in such a driving condition. Figure 9 shows the strain-electric field (S-E) loops measured by applying an AC electric field to a Mn-doped rhombohedral PIN-PMN-PT crystal sample under 0 MPa (a) or 10 MPa (b) compressive prestress, respectively [86]. Under 0 MPa prestress (Figure 9a), when the amplitude of the AC field is equal to or smaller than 5 kV/cm (roughly equal to its coercive field), the crystal sample showed a linear strain-field relationship with no concern of depoling/repoling. Beyond 5 kV/cm, the strain showed a more nonlinear response. When the AC field increased to 10 kV/cm, typical “butterfly”-shaped S-E loops occurred, indicating that domain reversal happened under each cycle of the AC field. Under 10 MPa prestress (Figure 9b), the negative strain peaks became rounded, as well as the maximum negative strain reduced sharply to nearly zero [86]. As a result, the coercive field declined sharply, which means that a much lower electric field and less energy are required to reverse the domains (depole/repole the crystal). In this measurement, depoling/repoling was initiated by an AC field with an amplitude of 2 kV/cm, which suggests that, if the crystal is driven by a low-frequency AC field under certain prestress, domain reversal-caused nonlinearity in the strain response may limit the amplitude of the driving AC field. For <001>-poled relaxor-PT crystals, as the compressive prestress aligns in the same direction as the electric field used for poling the crystal, it tends to destabilize the 4R domain configuration. However, it was demonstrated that the 4R domain configuration can be stabilized by a DC bias field applied in the same direction as that of the poling field. As shown in Figure 10, when a positive DC bias field was applied to the same crystal, the centers of the strain-field response loops were shifted toward the positive side of the electric field axis [86]. It is quite obvious that the range of the driving AC field, in which the crystal exhibited a linear strain response, was expanded to ± 4 kV/cm or ± 6 kV/cm, respectively, when a +2 kV/cm or +4 kV/cm DC bias was applied. The results indicated that the reduction of the linear

range of strain response caused by compressive prestress is recoverable if a positive DC bias is applied to the crystal.

Figure 9. S-E loops measured under a bipolar electric field and 0 MPa (a) and 10 MPa (b) uniaxial prestress (Mn:PIN-PMN-PT crystal in rhombohedral phase). Reprinted with permission from [86]. Copyright 2013 IEEE.

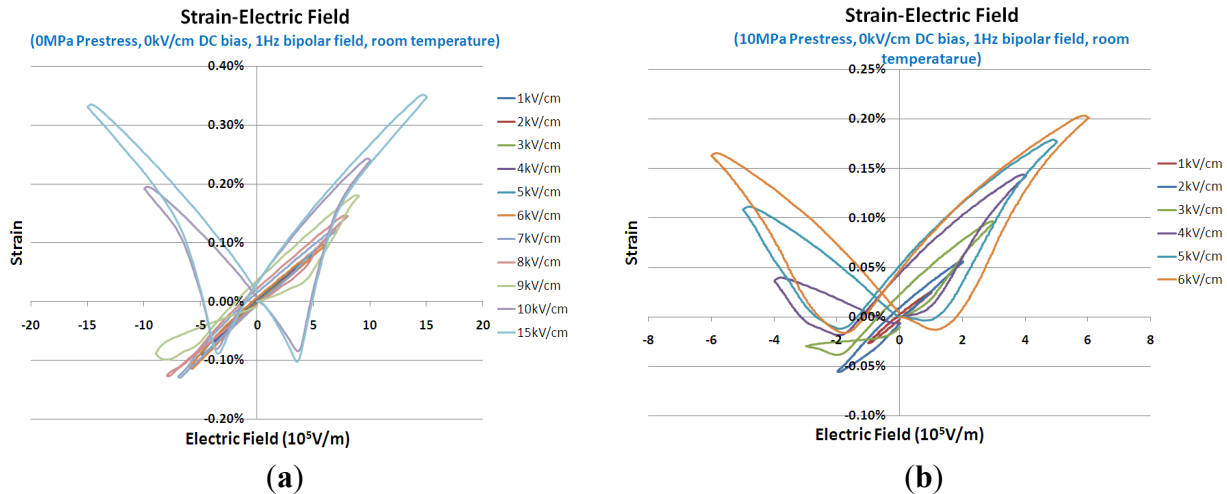
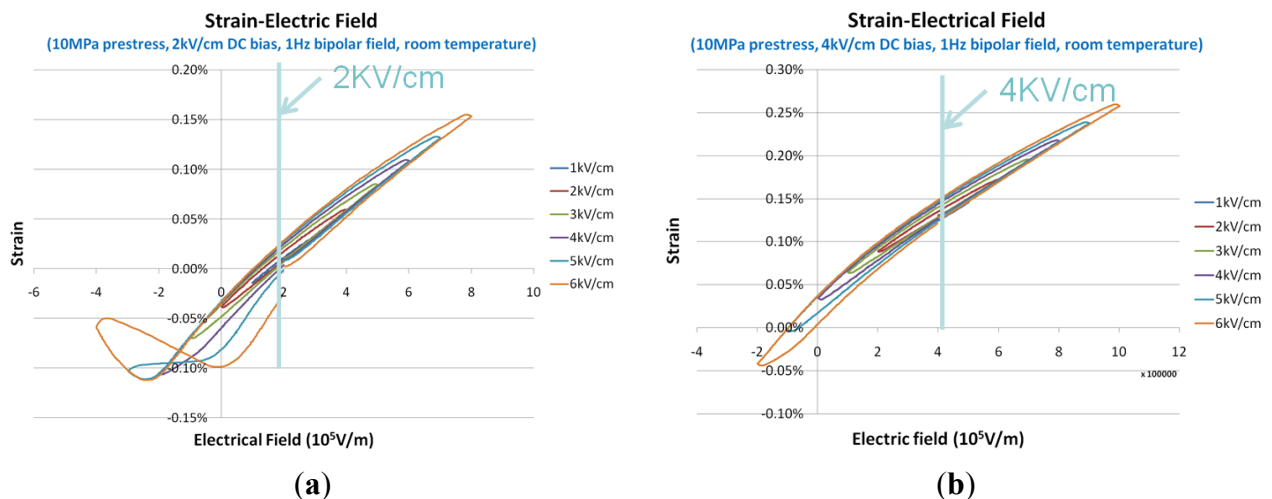


Figure 10. S-E loops of the same crystal sample as in Figure 9 measured under 10 MPa prestress and 2 kV/cm (a) and 4 kV/cm (b) external DC bias, respectively. Reprinted with permission from [86]. Copyright 2013 IEEE.

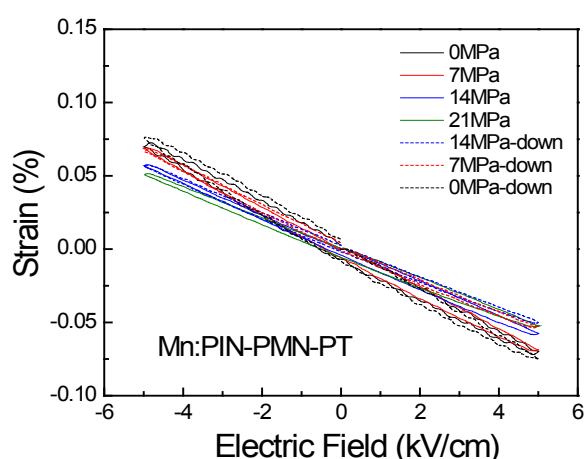


The <110>-poled relaxor-PT crystals have become more and more attractive for high power transducer design in recent years. When the relaxor-PT crystals operate in the <110>-poled transverse mode (32 mode, vibration along <001>), they possess very high d_{32} and k_{32} values; meanwhile, as the crystals are poled and driven through the thickness rather than the length, the required electric field to drive them is much lower than that for the 33 mode. Recent high field measurement also shows that <110>-poled relaxor-PT crystals may be more stable under the compressive prestress applied along their length (transverse compressive prestress). This study suggested that the transverse compressive

prestress will help stabilize the poling state until the electric field becomes large enough to induce the reversible rhombohedral-to-tetragonal phase transition [85].

Figure 11 shows the bipolar strain behavior of Mn:PIN-PMN-PT rhombohedral crystals at 5 kV/cm AC field and various stress levels [85]. It was found that all of the strain curves for the $\langle 110 \rangle$ -poled Mn:PIN-PMN-PT rhombohedra crystal are linear and non-hysteretic, demonstrating that no domain reversal occurs at 5 kV/cm. On the contrary, domain reversal happened at an AC field as low as 2 kV/cm for the $\langle 001 \rangle$ -poled Mn:PIN-PMN-PT crystal when it was under longitudinal compressive prestress, as implied by Figure 9b.

Figure 11. Bipolar strain behavior for Mn:PIN-PMN-PT crystals under different prestress levels. Reprinted with permission from [85]. Copyright 2013 AIP Publishing.



4. Conclusions

The successful flux growth of PMN-PT and PZN-PT single crystals started a new era in the exploration of the complex relaxor-based ferroelectric crystals. It is discovered that a variety of binary relaxor-PT and ternary relaxor-relaxor-PT/relaxor-PZ-PT crystals with claimed MPB compositions possess superior dielectric and piezoelectric properties to the conventional PZT ceramics, offering substantial advantages, such as a broad bandwidth, high sensitivity and/or high strain level for piezoelectric transduction and actuation applications [89].

In recent years, the vertical Bridgman growth of the large PMN-PT crystals led to a true breakthrough in the commercialization of relaxor-PT crystals. Currently, high-quality PMN-PT crystals with diameters up to 100 mm have become commercially available. However, as composition segregation is inevitable in the Bridgman growth method, further efforts are taken to improve the longitudinal composition homogeneity by applying alternative crystal growth techniques, including zone leveling, continuous feeding Bridgman growth and solid-state crystal growth.

To expand the operational temperature and electric field, a broad variety of binary relaxor-PT systems were investigated, among which, the PSN-PT, PIN-PT and PYN-PT with near MPB compositions were found to possess phase transition temperatures and coercive fields much higher than PMN-PT crystals. However, the obstacles encountered in the growth of large crystals hindered the further development of high Curie temperature (T_C), binary relaxor-PT crystals. In recent years, it was demonstrated that, by adding PMN-PT into some of the high T_C binary systems, the formed

PMN-PT-based ternary systems could have a relatively stable perovskite phase, offering the possibility of growing large crystals with a pure perovskite phase. Among the broadly studied ternary systems, substantial progress has been made on the growth of large PIN-PMN-PT crystals by the Bridgman process. PIN-PMN-PT crystals with a 75-mm diameter have become commercially available recently.

Compared to PZT ceramics, one of the distinguishing characteristics of the relaxor-based ferroelectric crystals is the strong anisotropy of their properties, which imposes new challenges in crystal characterization, as well as offering new opportunities for device design. The investigation of the orientation dependence of the rhombohedral relaxor-PT crystals indicated that, for the longitudinal mode (33 mode), the electromechanical coupling of $\langle 001 \rangle$ -poled crystals shows a similar value to that of $\langle 110 \rangle$ -poled crystals; however, the piezoelectric coefficient of $\langle 001 \rangle$ -poled crystal is much higher. For the transverse modes (d_{31} and d_{32} modes), significant anisotropy was observed for $\langle 110 \rangle$ -poled crystals. Optimal transverse properties were found for the crystals polarized through $\langle 110 \rangle$ with vibration along $\langle 001 \rangle$ (32 mode), possessing values of electromechanical coupling and the piezoelectric coefficient similar to those of the $\langle 001 \rangle$ -poled longitudinal mode. Another challenge in the characterization of relaxor-PT crystals is that their properties can be influenced largely by multiple factors, including temperature, preloading stress and electric field, especially when the crystals are engaged in applications that require a high power output. It was observed that uniaxial compressive prestress, which is usually applied to the crystal elements in high power devices to prevent them from fracturing under tensile stress, strongly affects the piezoelectric performance of the relaxor-PT-based crystals along different poling orientations. However, systematic studies are needed in this critical field to determine the operational domains of these crystals for high power applications.

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Author Contributions

The original work in this paper was done by both authors, with Jun Luo focusing on the crystal growth and Shujun Zhang focusing on the characterization. The paper was written by Jun Luo through discussion with Shujun Zhang.

Conflicts of Interest

The authors declare no conflict of interest.

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